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PLANETARY GEARING

Milton F. Lindgren and Victor W. Peterson, Indianapolis, Ind., assignors to General Motors Corporation, Detroit, Mich., a corporation of Delaware

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Our invention relates generally to planetary gearing and more particularly to planetary gearing having herringbone or self-aligning type gear teeth. Our planetary gearing is especially suitable for, but not limited to, use as a reduction gear unit between a gas turbine engine and a propeller.

In such a reduction gear unit as in practically all machinery, it is desirable to have the parts capable of axial adjustment. This is desirable among other reasons because the parts will usually experience differential thermal expansion. The differential thermal expansion may be due to use of different materials throughout the gear box unit, different temperature levels at different points in the gear box unit or a variety of reasons. In a reduction gear box for a turboprop, the torque loadings on the gear teeth are usually relatively high and it is desirable to have the axial adjustment made without additionally loading the already highly loaded gear teeth.

Our invention is directed primarily toward providing this capability in a planetary gear set. We are primarily concerned with suitably mounting a planetary gear set of the herringbone or self-aligning type within a housing while at the same time accommodating for differential thermal expansion or axial adjustment of the elements thereof without adding any load to the gear teeth of the gear train.

Other objects and features of the invention will become apparent to those skilled in the art as the disclosure is made in the following detailed description of a preferred embodiment of the invention as illustrated in the accompanying sheet of drawings in which:

FIGURE 1 is a view in cross section of a gear train mounted in its housing in accordance with our invention.

FIGURE 2 is a section taken along the line 2—2 of FIGURE 1 and looking in the direction of the arrows.

FIGURE 3 is a section taken along the line 3—3 of FIGURE 1 and looking in the direction of the arrows.

Our reduction gear includes a housing generally indicated at 12. The housing 12 is made in two main sections 14 and 16 which are bolted together so as to mount a heavy vertical wall 18 between them. A pinion gear 20 has its forward end journaled in a roller bearing 22 mounted in the lower end of the vertical wall 18. The aft end of the pinion gear 20 is journaled in a second roller bearing 24 mounted in the rear vertical wall 17 of the housing 12. Input shaft 26 extends through the wall 17 into the hollow annular pinion gear 20 and is splined to it at its forward end 28. An accessory drive gear 30 is secured to the forward end of the input shaft 28 ahead of the pinion gear 20. The gear 30 meshes with a second gear (not shown) to drive an accessory and as such is a power take-off. The manner of connecting the accessory drive gear 30 to the input shaft 26 can best be understood by reference to FIGURE 2 in connection with FIGURE 1.

As is evident from FIGURE 1, the gear 30 has an integral axially extending portion 32 which has its inner end disposed between the pinion gear 20 and the input shaft 26. Adjacent this inner end is an inwardly extending flange 34 which is castellated to provide circumferentially spaced slots 36. This is best seen in FIGURE 2. Lugs 38 extending axially from the input shaft 26 are disposed in the slots 36 and together with the castellations present a continuous inner circumferential surface. The continuous

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inner circumferential surface has a radial groove formed by aligned grooves in the individual castellations 34 and the lugs 38. The radial groove receives a snap ring 40 which thus connects the parts. A cuplike member 42 is nested in the input shaft 26 between the snap ring 40 and an internal shoulder on the input shaft 26. The member 42 serves as an oil puddler abutment for the inside of shaft 26.

The gear 32 being connected to the shaft 26 also positively locates pinion gear 20 axially with respect to shaft 26 since the internal splines 28 on the gear 20 are sandwiched between the inner end of the gear 32 and a radial boss 29 on the shaft 26. The shaft 26 in turn is axially fixed with respect to the housing 12 by a thrust bearing (not shown). The pinion gear 20 is seen to comprise a pair of axially spaced circumferential rows of teeth 44 and 46, respectively. The teeth on this gear as well as the teeth on the remaining gears are of the herringbone type, that is, the left row 44 has a lead opposite to the lead of the right row. This gives a self-aligning feature to all of the gears.

The pinion gear 20 meshes with a large main gear 48 which has an integral hollow shaft 50. The shaft 50 carries the inner races of roller bearings 52 and 54 at its forward and aft ends, respectively. The outer race of the roller bearing 52 is mounted in the vertical wall 18 while the outer race of the roller bearing 54 is mounted in the rear housing wall 17. Thus the gear 48 and shaft 50 is journaled in the housing 12. It is fixed axially with respect to the housing 12 by being in mesh with axially fixed pinion 20 through herringbone gear teeth.

Noting the detail of the aft roller bearing mount 54, we see that the outer race is clamped between a pair of members 56 and 58 which are bolted to the rear housing wall 17. The rightmost member 58 is cup shaped and has an integral axial flange 60 at the middle of its bottom wall. The inner surface of flange 60 is splined and receives mating splines on an oil supply tube 62 to nonrotatably mount it. The oil supply tube communicates with an oil supply chamber 64 in the rear wall 17 of the housing 12 with the bottom wall of the cupped member 58 sealingly engaging the back wall 17 to prevent leakage of oil as it flows from chamber 64 into tube 62. The tube 62 extends to the left and is disposed within shaft 50 and a short coupling shaft 66.

The short hollow coupling shaft 66 connects the main gear 48 with a sun gear 68. It is drivingly connected to the main gear shaft 50 by mating internal and external splines 70 on the respective members. The coupling shaft 66 and the main gear shaft 50 are fixed axially by a buried Spiralex snap ring 72 (see FIGURES 1 and 3). The inner circumference of the forward end of the integral main gear shaft 50 is grooved at 74. The mid portion of the outer circumference of the coupling shaft 66 has an outward boss 75 which contains a like groove 76. The face of the shaft 50 is slotted at 78 to the depth of the groove 74. Likewise the face of the boss 75 on the coupling shaft 66 is slotted at 80 to a depth of the groove 76. In coupling the members 66 and 50, they are adjusted so that the grooves 74 and 76 are in axial alignment and the slots 78 and 80 are in circumferential alignment. The Spiralex snap ring 72 is then fed through the opening created by the aligned slots 78 and 80 into the aligned grooves 74 and 76. The parts are thus connected axially. It is to be understood that while we have shown two diametrically opposed pairs of slots 78 and 80, two pairs of slots are not necessary. The pairs of slots are utilized for balance purposes only since a single pair of slots is all that is required to make the connection.

As stated above, the sun gear 68 is connected to the coupling shaft 66 which in turn is connected to the main